

RAPTOR equation summary

F. Felici, f.felici@tue.nl

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1 Definitions

$$\begin{aligned} V' &= \frac{\partial V}{\partial \rho}, \quad G_1 = \langle (\nabla \rho)^2 \rangle, \quad G_2 = \frac{V'}{4\pi^2} \left\langle \frac{(\nabla \rho)^2}{R^2} \right\rangle. \\ g_1 &= \langle (\nabla V)^2 \rangle, \quad g_2 = \left\langle \frac{(\nabla V)^2}{R^2} \right\rangle, \quad g_3 = \left\langle \frac{1}{R^2} \right\rangle. \\ \rho_e &= \sqrt{\Phi_b / \pi B_0}, \quad F = RB_\phi \\ j_{ni} &= \frac{\langle \mathbf{j}_{ni} \cdot \mathbf{B} \rangle}{B_0} \end{aligned}$$

2 Flux transport

Flux surface averaged ohm's law in general form:

$$\sigma_{\parallel} \left. \frac{\partial \Phi}{\partial t} \right|_{\psi} = \frac{F^2}{2\pi\mu_0} \frac{\partial}{\partial \psi} \left[\frac{g_2}{F} \frac{\partial \psi}{\partial V} \right] - \frac{\partial V}{\partial \psi} \langle \mathbf{j}_{ni} \cdot \mathbf{B} \rangle \quad (1)$$

We can then re-write this with ψ or Φ or ρ as independent variable:

2.1 Φ

$\hat{\Phi} = \Phi / \Phi_b$, always $[0,1]$

$$\sigma_{\parallel} \left(\left. \frac{\partial \psi}{\partial t} \right|_{\hat{\Phi}} - \frac{\hat{\Phi} \dot{\Phi}_b}{\Phi_b} \frac{\partial \psi}{\partial \hat{\Phi}} \right) = \frac{F^2}{4\pi^2\mu_0\Phi_b^2} \frac{\partial}{\partial \hat{\Phi}} \left[g_2 g_3 \frac{\partial \psi}{\partial \hat{\Phi}} \right] - \frac{1}{\Phi_b} \frac{\partial V}{\partial \hat{\Phi}} \langle \mathbf{j}_{ni} \cdot \mathbf{B} \rangle \quad (2)$$

Which is equal to E. Fable's notes.

2.2 ρ

$\rho = \sqrt{\Phi / \pi B_0}$, $d\Phi = 2\pi B_0 \rho d\rho$, and $\hat{\rho} = \sqrt{\hat{\Phi}} = \sqrt{\Phi / \Phi_b}$, $d\Phi = 2\Phi_b \hat{\rho} d\hat{\rho}$

$$\sigma_{\parallel} \left(\left. \frac{\partial \psi}{\partial t} \right|_{\rho} - \frac{\rho \dot{B}_0}{2B_0} \frac{\partial \psi}{\partial \rho} \right) = \frac{F^2}{16\pi^4\mu_0 B_0^2 \rho} \frac{\partial}{\partial \rho} \left[\frac{g_2 g_3}{\rho} \frac{\partial \psi}{\partial \rho} \right] - \frac{1}{2\pi\rho} \frac{\partial V}{\partial \rho} \frac{\langle \mathbf{j}_{ni} \cdot \mathbf{B} \rangle}{B_0} \quad (3)$$

Which is equal to [1] since $\frac{G_2}{J} = \frac{R_0}{16\pi^4} \frac{g_2 g_3}{\rho}$

$$\sigma_{\parallel} \left(\left. \frac{\partial \psi}{\partial t} \right|_{\hat{\rho}} - \frac{\hat{\rho} \dot{\Phi}_b}{2\Phi_b} \frac{\partial \psi}{\partial \hat{\rho}} \right) = \frac{F^2}{16\pi^2\mu_0\Phi_b^2\hat{\rho}} \frac{\partial}{\partial \hat{\rho}} \left[\frac{g_2 g_3}{\hat{\rho}} \frac{\partial \psi}{\partial \hat{\rho}} \right] - \frac{B_0}{2\Phi_b\hat{\rho}} \frac{\partial V}{\partial \hat{\rho}} \frac{\langle \mathbf{j}_{ni} \cdot \mathbf{B} \rangle}{B_0} \quad (4)$$

3 Thermal transport

$$V' \frac{\partial}{\partial t} [n_e T_e] = \frac{\pi B_0}{\Phi_b} \frac{\partial}{\partial \hat{\rho}} \frac{g_1 n_e}{V'} \chi_e \frac{\partial T_e}{\partial \hat{\rho}} + V' P_e \quad (5)$$

4 Finite Element forms

$$\sigma_{\parallel} \left(\frac{\partial \psi}{\partial t} \Big|_{\hat{\rho}} - \frac{\hat{\rho} \dot{\Phi}_b}{2\Phi_b} \frac{\partial \psi}{\partial \hat{\rho}} \right) = \frac{F^2}{16\pi^2 \mu_0 \Phi_b^2 \hat{\rho}} \frac{\partial}{\partial \hat{\rho}} \left[\frac{g_2 g_3}{\hat{\rho}} \frac{\partial \psi}{\partial \hat{\rho}} \right] - \frac{B_0}{2\Phi_b \hat{\rho}} \frac{\partial V}{\partial \hat{\rho}} j_{ni} \quad (6)$$

is rewritten as

$$\frac{16\pi^2 \mu_0 \Phi_b^2 \hat{\rho} \sigma_{\parallel}}{F^2} \frac{\partial \psi}{\partial t} \Big|_{\hat{\rho}} = \frac{\partial}{\partial \hat{\rho}} \left[\frac{g_2 g_3}{\hat{\rho}} \frac{\partial \psi}{\partial \hat{\rho}} \right] + \frac{16\pi^2 \mu_0 \Phi_b^2 \hat{\rho} \sigma_{\parallel}}{F^2} \frac{\hat{\rho} \dot{\Phi}_b}{2\Phi_b} \frac{\partial \psi}{\partial \hat{\rho}} - \frac{16\pi^2 \mu_0 \Phi_b}{2F^2} \frac{\partial V}{\partial \hat{\rho}} \langle \mathbf{j}_{ni} \cdot \mathbf{B} \rangle \quad (7)$$

or

$$m_{\psi} \frac{\partial \psi}{\partial t} = a_{\psi} \frac{\partial \psi}{\partial \hat{\rho}} + \frac{\partial}{\partial \hat{\rho}} d_{\psi} \frac{\partial \psi}{\partial \hat{\rho}} + s_{\psi} \quad (8)$$

with

$$m_{\psi} = 16\pi^2 \mu_0 \hat{\rho} \frac{\Phi_b^2 \sigma_{\parallel}}{F^2} \quad (9)$$

$$a_{\psi} = 16\pi^2 \mu_0 \hat{\rho}^2 \frac{\dot{\Phi}_b \Phi_b \sigma_{\parallel}}{2F^2} \quad (10)$$

$$d_{\psi} = \frac{g_2 g_3}{\hat{\rho}} \quad (11)$$

$$s_{\psi} = -8\pi^2 \mu_0 \frac{B_0 \Phi_b}{F^2} \frac{\partial V}{\partial \hat{\rho}} j_{ni} \quad (12)$$

$$(13)$$

Now write ψ as a sum of spatial basis functions

$$\psi(\rho, t) = \sum_{\alpha=1}^{n_{sp}} \Lambda_{\alpha}(\hat{\rho}) \hat{y}_{\alpha}(t) \quad (14)$$

then the weak form, after projection on Λ_b and integration by parts is

$$\sum_{\alpha=1}^{n_{sp}} \frac{d\hat{y}_{\alpha}(t)}{dt} \int_0^1 m \Lambda_{\beta} \Lambda_{\alpha} d\hat{\rho} = \sum_{\alpha=1}^{n_{sp}} \hat{y}_{\alpha} \int_0^1 a_{\psi} \Lambda_{\beta} \frac{\partial \Lambda_{\alpha}}{\partial \hat{\rho}} d\hat{\rho} \quad (15)$$

$$- \sum_{\alpha=1}^{n_{sp}} \hat{y}_{\alpha} \int_0^1 d_{\psi} \frac{\partial \Lambda_{\beta}}{\partial \hat{\rho}} \frac{\partial \Lambda_{\alpha}}{\partial \hat{\rho}} d\hat{\rho} + \left[d_{\psi} \Lambda_{\beta} \frac{\partial \psi}{\partial \hat{\rho}} \right]_0^1 + \int_0^1 \Lambda_{\beta} s_{\psi} d\hat{\rho} \quad (16)$$

which gives the matrix form

$$\mathbf{M}_{\psi} \frac{d\hat{\psi}}{dt} = (-\mathbf{D}_{\psi} + \mathbf{A}_{\psi}) \hat{\psi} + \mathbf{l} + \mathbf{s} \quad (17)$$

The boundary term \mathbf{l} contains only the last element

$$d_{\psi} \Lambda_{\beta} \frac{\partial \psi}{\partial \hat{\rho}} \Big|_{\rho=1} = \frac{g_2 g_3}{\hat{\rho}} \frac{\partial \psi}{\partial \hat{\rho}} \Big|_{\rho=1} = \frac{16\pi^3 \mu_0 \Phi_b}{R_0 B_0} I_p \quad (18)$$

5 Other quantities

$$\iota = \frac{1}{q} = \frac{\partial \psi}{\partial \Phi} = \frac{\partial \rho}{\partial \Phi} \frac{\partial \hat{\rho}}{\partial \rho} \frac{\partial \psi}{\partial \hat{\rho}} = \frac{1}{2\Phi_b \hat{\rho}} \frac{\partial \psi}{\partial \hat{\rho}} \quad (19)$$

$$I_p = \frac{F}{8\pi^3 \mu_0 \Phi_b} \frac{g_2 g_3}{2\hat{\rho}} \frac{\partial \psi}{\partial \hat{\rho}} = \frac{g_2 g_3}{8\pi^3 \mu_0} \frac{F}{q} \quad (20)$$

$$j_{tor} = \frac{R_0}{2\pi \mu_0} \frac{\partial}{\partial V} g_2 \frac{\partial \psi}{\partial V} = \frac{R_0}{2\pi \mu_0 \hat{V}'} \frac{\partial}{\partial \hat{\rho}} \frac{g_2}{\hat{V}'} \frac{\partial \psi}{\partial \hat{\rho}} \quad (21)$$

References

- [1] G. V. Pereverzev and P.N. Yushmanov. ASTRA Automated System for TRansport Analysis in a Tokamak. Technical Report 5/98, IPP Report, February 2002.